

## Homework 4

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$$1) \Psi(r, \theta) = U r^2 \sin 2\theta$$

$$r = x^2 + y^2$$

$$\sin 2\theta = 2 \sin \theta \cos \theta$$

$$= \frac{2y}{\sqrt{x^2 + y^2}} \cdot \frac{x}{\sqrt{x^2 + y^2}} = \frac{2xy}{x^2 + y^2}$$

$$\Psi(x, y) = \frac{U(x^2 + y^2) 2xy}{x^2 + y^2} = 2xyU$$

$$\Psi(x, y) = 2xyU$$

$$u = \frac{\partial \Psi}{\partial y} = 2xU \quad ; \quad v = -\frac{\partial \Psi}{\partial x} = -2yU$$

Boundary Conditions

1. at  $x = 0$ ,  $u = 0$  (symmetry + flow velocity)

$$u|_{x=0} = 2 \times 0 \times U = 0 \quad \text{satisfied}$$

2. at  $y = 0$ ,  $v = 0$

$$v|_{y=0} = -2 \times 0 \times U = 0 \quad \text{satisfied}$$

No slip boundary cant be applied as this is assumed to be ideal fluid, so it can slip on the boundaries

$$u = 2xU$$

$$v = -2yU$$

$$\nabla \times \vec{V} = 0 \quad \text{Irrotational flow}$$

So Bernoulli's theorem can be applied between any two points.

Applying Bernoulli's equation

$$P_0 + 0 = P_x + \frac{1}{2} \rho |\vec{v}|^2$$

$$\Rightarrow P_x = P_0 + \frac{1}{2} \rho [(2xU)^2 + (-2yU)^2]$$

$$P = P_0 - 2\rho U^2(x^2 + y^2)$$

b) Navier-Stokes for 2D flows & no body forces

$$\rho \left( \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} \right) = -\frac{\partial P}{\partial x} + \mu \left( \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right) \quad x$$

$$\rho \left( \frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} \right) = -\frac{\partial P}{\partial y} + \mu \left( \frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} \right) \quad y$$

$$\frac{x}{\rho} \rho (0 + (2xU)(2U) + 0) = -\frac{\partial P}{\partial x} + \mu(0+0)$$

$$LHS = 4U^2 x \rho \quad , \quad RHS = 2\rho U^2(2x)$$

$$= 4\rho U^2 x$$

$\therefore LHS = RHS$

$$\frac{y}{\rho} LHS = \rho [0 + 0 + (-2yU)(-2U)] \quad RHS = -\frac{\partial P}{\partial y} + \mu(0)$$

$$= 4yU^2 \rho \quad = 4\rho yU^2$$

$$LHS = RHS$$

Hence the former velocity & pressure satisfy the Navier Stokes equations

BC for the viscous problem, (in addition to previous BCs)  
No-slip BC on  $y=0$

$$u|_{y=0} = 0$$

But  $u|_{y=0} = 2xU \neq 0$  so not satisfied

c)  $u = 2Ux f'$  where  $f$  is a function of  $y$

Continuity Equation:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$

$$\frac{\partial v}{\partial y} = -2Uf'$$

$$v = -2Uf$$

based on B.C.s.

① No normal velocity at boundary  
 $v|_{y=0} = 0 \Rightarrow f(0) = 0$

② No slip at boundary  
 $u|_{y=0} = 0 \Rightarrow f'(0) = 0$

③ At large  $y$  (far away from boundary)  
 $u|_{y \rightarrow \infty} = 2xU \Rightarrow f'(\infty) = 1$  .  $v|_{y \rightarrow \infty} = -2uf \Rightarrow f(\infty) = y$   
Both are same

d)  $y$ -momentum with  $u = 2xUf'$  ,  $v = -2Uf$

$$\rho u \frac{\partial v}{\partial x} + \rho v \frac{\partial v}{\partial y} = -\frac{\partial p}{\partial y} + \mu \left( \frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} \right)$$

$$\Rightarrow \rho (2xUf')(0) + \rho (-2Uf)(-2Uf') = -\frac{\partial p}{\partial y} + \mu (0 + (-2Uf''))$$

$$\Rightarrow 4U^2 f f' \rho = -\frac{\partial p}{\partial y} = -2U\mu f''$$

$$\Rightarrow \frac{\partial p}{\partial y} = -4U^2 f f' \rho + 2U\mu f''$$

RHS is only function of  $y$  so integrating directly

$$p = -2U^2 \rho f^2 - 2U\mu f' + m(x)$$

Recovery of old flow at  $y \rightarrow \infty$

(c)

so  $P$  should approach old pressure value

$$f. P_0 - 2\rho U^2(x^2 + y^2) = -2U^2\rho y^2 - 2Uu + o_n(1)$$

(Since  $f(\infty) = y$  &  $f'(\infty) = 1$ )

$$o_n(x) = P_0 - 2\rho U^2 x^2 + 2Uu$$

$$\therefore \boxed{P(x, y) = P_0 - 2\rho U^2 f^2 + 2uU(1-f') - 2\rho U^2 x^2}$$

e) X-momentum

$$\rho \left( u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} \right) = -\frac{\partial P}{\partial x} + \mu (0 + 2Ux f''')$$

$$\Rightarrow \rho \cdot (2xUf'') (2Uf') - \rho (2Uf) (2Ux f''') = -\frac{\partial P}{\partial x} + 2\mu Ux f'''$$

$$\Rightarrow 4\rho x U^2 (f')^2 - 4U^2 x \rho f f'' = -2\rho U^2 (2x) + 2\mu Ux f'''$$

Cancelling  $x$ , and dividing by  $4\rho U^2$  on all sides

$$(f')^2 - f f'' = 1 + \frac{\nu}{2U} f''' \quad (\text{where } \nu = \frac{\mu}{\rho})$$

$$\boxed{\frac{\nu}{2U} f''' + f f'' - (f')^2 + 1 = 0}$$

BCs from (c) part

①  $f(\infty) = y$

②  $f'(0) = 0$

③  $f(0) = 0$

This is a third order ODE in  $f$  with 3 BCs and it is non-linear. It can be solved numerically with Runge-Kutta method or any such method.

$$2) \frac{u}{U} = a + b\left(\frac{y}{\delta}\right) + c\left(\frac{y}{\delta}\right)^2$$

BCs given

$$\textcircled{1} u=0 \text{ at } y=0$$

$$\Rightarrow 0 = a + 0 + 0$$

$$\Rightarrow a = 0$$

$$\textcircled{2} u=U \text{ at } y=\delta$$

$$\Rightarrow 1 = 0 + b + c$$

$$\Rightarrow b + c = 1$$

$$\textcircled{3} \frac{\partial u}{\partial y} = 0 \text{ at } y = \delta$$

$$\frac{1}{U} \frac{\partial u}{\partial y} = \frac{b}{\delta} + \frac{c}{\delta^2} 2y$$

$$\text{at } y = \delta$$

$$\frac{b}{\delta} + \frac{2c}{\delta} = 0$$

$$b + 2c = 0$$

$$\therefore \boxed{b = 2, c = -1}$$

$$\boxed{u = \frac{U 2y}{\delta} - \frac{U y^2}{\delta^2}}$$

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = U \frac{dU}{dx} + \nu \frac{\partial^2 u}{\partial y^2}$$

for flat plate, these equations when integrated and combined

$$\frac{d}{dx} \int_0^{\infty} u(V-u) dy = \frac{C_0}{\rho}$$

$$\Rightarrow \int_0^{\delta} u(V-u) dy = U^2 \int_0^{\delta} \left(\frac{2y}{\delta} - \frac{y^2}{\delta^2}\right) \left(1 - \frac{2y}{\delta} + \frac{y^2}{\delta^2}\right) dy$$

$$\boxed{\frac{y}{\delta} = p}$$

$$dy = \delta dp$$

$$\Rightarrow \delta U^2 \int_0^1 (2p - p^2)(1 - 2p + p^2) dp$$

$$= \delta U^2 \int_0^1 (2p - 4p^2 + 2p^3 - p^2 + 2p^3 - p^4) dp$$

$$= \delta U^2 \left[ \frac{2p^2}{2} - \frac{4p^3}{3} + \frac{2p^4}{4} - \frac{p^3}{3} + \frac{2p^4}{4} - \frac{p^5}{5} \right]_0^1$$

$$= \delta U^2 \left( 1 - \frac{4}{3} + \frac{1}{2} - \frac{1}{3} + \frac{1}{2} - \frac{1}{5} \right)$$

$$= \frac{2}{15} \delta U^2$$

$$\underline{LHS} = \frac{d}{dx} \left( \frac{2}{15} \delta U^2 \right) = \boxed{\frac{2U^2 d\delta}{15 dx}}$$

$$\underline{RHS}, \frac{\tau_0}{\rho} = \nu \left( \frac{\partial u}{\partial y} \right) \Big|_{y=0} = \nu U \left( \frac{2}{\delta} - \frac{2Uy}{\delta^2} \right) \Big|_{y=0} = \frac{2\nu U}{\delta}$$

$$\underline{LHS} = \underline{RHS} \Rightarrow \frac{2U^2 d\delta}{15 dx} = \frac{2\nu U}{\delta}$$

$$\Rightarrow \int \delta d\delta = \int 15 \left( \frac{\nu}{U} \right) dx$$

$$\Rightarrow \frac{\delta^2}{2} = 15 \frac{\nu}{U} x$$

$$\delta = \sqrt{30 \frac{\nu x}{U}} \Rightarrow \delta = 5.4772 \sqrt{\frac{\nu x}{U}}$$

$$\Rightarrow \frac{\delta}{x} = \frac{5.4772}{\sqrt{Re}}$$

Blasius  $\Rightarrow \delta = 5 \sqrt{\frac{\nu x}{U}}$   
 So  $\delta$  for quadratic assumption is the highest among Blasius & cubic assumption  
 Momentum thickness ( $\theta$ ),  $U^2 \theta = \int_0^\infty u(U-u) dy$

$$\Rightarrow U^2 \theta = \frac{2U^2 \delta}{15} \Rightarrow \theta = \frac{2\delta}{15} = \frac{2}{15} \sqrt{30 \frac{\nu x}{U}} \Rightarrow \frac{\theta}{x} = \frac{2\sqrt{30}}{15} \frac{1}{\sqrt{Re}} = \boxed{\frac{0.7303}{\sqrt{Re}}}$$

$$\text{Blasius} \Rightarrow \frac{\theta}{x} = \frac{0.664}{\sqrt{Re}}, \text{ cubic} \Rightarrow \frac{\theta}{x} = \frac{0.646}{\sqrt{Re}}$$

As expected from  $\frac{\delta}{x}$ ,  $\frac{\theta}{x}$  for quadratic is more than both Blasius & cubic