

# *Computational Structural Mechanics and Dynamics*

Master of Science in Computational Mechanics  
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*Homework 5*

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**Problem 5.1**

Consider a three-node bar element referred to the natural coordinate  $\xi$ . The two end nodes and the mid node are identified as 1, 2 and 3 respectively. The natural coordinates of nodes 1, 2 and 3 are  $\xi = -1$ ,  $\xi = 1$  and  $\xi = 0$ , respectively. The variation of the shape functions  $N_1(\xi)$ ,  $N_2(\xi)$  and  $N_3(\xi)$  is sketched in the figure below. These functions must be quadratic polynomials in  $\xi$ :

$$N_1^e(\xi) = a_0 + a_1\xi + a_2\xi^2 \quad N_2^e(\xi) = b_0 + b_1\xi + b_2\xi^2 \quad N_3^e(\xi) = c_0 + c_1\xi + c_2\xi^2$$

- (a) Determine the coefficients  $a_0, \dots, c_2$  using the node value conditions depicted in figure. For example  $N_1^e = 1$  for  $\xi = 1$  and 0 for the rest of natural coordinates. The rest of the nodes follow the same scheme.

$$\begin{aligned} N_1^e(-1) = a_0 - a_1 + a_2 = 1 & \quad N_2^e(-1) = b_0 - b_1 + b_2 = 0 & \quad N_3^e(-1) = c_0 - c_1 + c_2 = 0 \\ N_1^e(0) = a_0 = 0 & \quad N_2^e(0) = b_0 = 0 & \quad N_3^e(0) = c_0 = 1 \\ N_1^e(+1) = a_0 + a_1 + a_2 = 0 & \quad N_2^e(+1) = b_0 + b_1 + b_2 = 1 & \quad N_3^e(+1) = c_0 + c_1 + c_2 = 0 \end{aligned}$$

*Solving the linear system we can know the values for  $a_0, \dots, c_2$ :*

$$N_1^e(\xi) = \frac{1}{2}\xi(1 - \xi) \quad N_2^e(\xi) = \frac{1}{2}\xi(1 + \xi) \quad N_3^e(\xi) = 1 - \xi^2$$

- (b) Verify that their sum is identically one.

$$N_1 + N_2 + N_3 = \frac{1}{2}\xi - \frac{1}{2}\xi + \frac{1}{2}\xi^2 + \frac{1}{2}\xi^2 - \xi^2 + 1 = 1$$

- (c) Calculate their derivatives respect to the natural coordinates.

$$\frac{\partial N_1}{\partial \xi} = \xi - \frac{1}{2} \quad \frac{\partial N_2}{\partial \xi} = \xi + \frac{1}{2} \quad \frac{\partial N_3}{\partial \xi} = 2\xi$$

**Problem 5.2**

A five node quadrilateral element has the nodal configuration shown in the figure with two perspective views of  $N_1^e$  and  $N_5^e$ . Find five shape functions  $N_i^e, i = 1, \dots, 5$  that satisfy compatibility and also verify that their sum is unity.

- First of all, the shape function  $N_5$  is obtained by construction as:

$$N_5 = C_5 L_{12} L_{23} L_{34} L_{41} \implies C_5 (1 - \xi)(1 - \eta)(1 + \xi)(1 + \eta)$$

- Substituting the coordinates (0, 0) corresponding with  $N_5$  location; the value of  $C_5$  is found as 1, arising the final shape-function:

$$N_5 = (1 - \xi^2)(1 - \eta^2)$$

- The given shape-functions for the corner nodes are the following:

$$N_1 = \frac{1}{4}(1 - \xi)(1 - \eta) \quad N_2 = \frac{1}{4}(1 + \xi)(1 - \eta) \quad N_3 = \frac{1}{4}(1 + \xi)(1 + \eta) \quad N_4 = \frac{1}{4}(1 - \xi)(1 + \eta)$$

- It is obtained a general shape function for all the nodes of the element:

$$N_i = \frac{1}{4}(1 + \xi\xi_i)(1 + \eta\eta_i) + \alpha N_5$$

- The value of  $\alpha$  can be found substituting the coordinates of node 5 (0,0) into any of the shape functions and equalize to zero. For instance, substitution of  $\xi = \eta = 0$  in  $N_1$  yields:

$$N_1 = \frac{1}{4}(1 - \xi)(1 - \eta) + \alpha(1 - \xi^2)(1 - \eta^2) \quad (1)$$

$$= \frac{1}{4} + \alpha = 0 \quad \implies \quad \alpha = -\frac{1}{4} \quad (2)$$

- In addition, the summation of all shape functions is equal to 1:

$$\begin{aligned} N_1 + N_2 + N_3 + N_4 + N_5 &= \frac{1}{4}(1 - \xi)(1 - \eta) + \frac{1}{4}(1 + \xi)(1 - \eta) + \frac{1}{4}(1 + \xi)(1 + \eta) + \frac{1}{4}(1 - \xi)(1 + \eta) + 4\alpha N_5 + N_5 \\ \implies \frac{1}{4}(1 - \xi - \eta + \xi\eta) + \frac{1}{4}(1 + \xi - \eta - \xi\eta) + \frac{1}{4}(1 + \xi + \eta + \xi\eta) + \frac{1}{4}(1 - \xi + \eta - \xi\eta) - N_5 + N_5 &= 1 \end{aligned}$$


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### Problem 5.3

Which minimum integration rules of Gauss-product type gives a rank sufficient stiffness matrix for these elements:

Before start computing the gauss points we are going to define the following values, taking account we are in 3D space.

$$n_F = 3n \quad \text{number of element DoF} \quad (3)$$

$$n_R = 6 \quad \text{number of independent rigid body modes} \quad (4)$$

$$n_E = 6 \quad \text{order of } E \text{ stress - strain matrix} \quad (5)$$

$$n_G = \quad \text{number of Gauss points in integration rule for } K \quad (6)$$

$$r = \quad \text{actual rank stiffness matrix} \quad (7)$$

1. the 8-node hexahedron

$$r_{min} = 18 \quad d = 0 \quad \text{with } \mathbf{3} \text{ Gauss points}$$

2. the 20-node hexahedron

$$r_{min} = 54 \quad d = 0 \quad \text{with } \mathbf{9} \text{ Gauss points}$$

3. the 27-node hexahedron

$$r_{min} = 75 \quad d = 0 \quad \text{with } \mathbf{13} \text{ Gauss points}$$

4. the 64-node hexahedron

$$r_{min} = 186 \quad d = 0 \quad \text{with } \mathbf{31} \text{ Gauss points}$$