

# LAB REPORT - 6

## INCOMPRESSIBLE FLOW MATLAB EXERCISES

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### 1

#### 1.1

The L2 error norm of the pressure, the H1 error semi norm of the velocity and the L2 error norm of velocity were computed for  $N \times N$  elements where  $N = 2, 4, 8, 16, 24, 32$ .

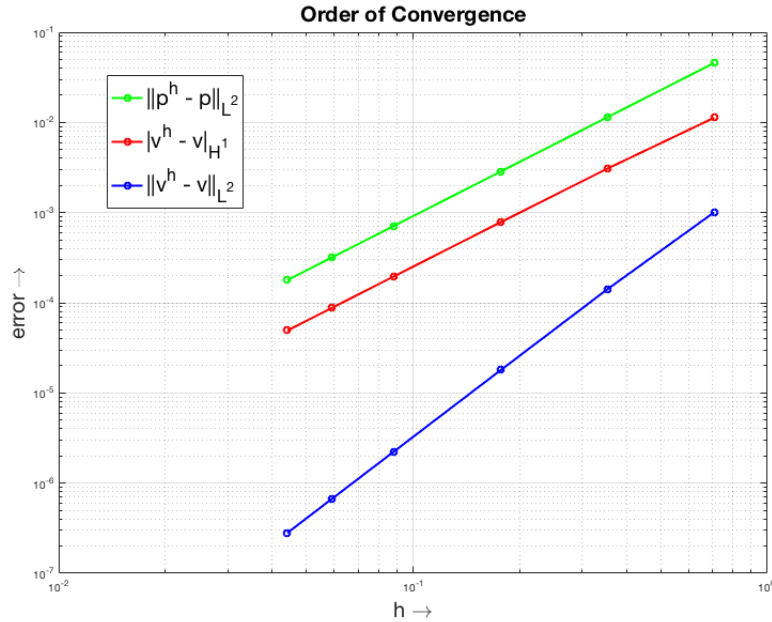


Fig 1. Order of Convergence -  $Q_2Q_1$  element

Expected order of 3 was observed for  $L^2$  error of the velocity because of the use of  $Q_2$  elements to interpolate velocity. Expected order of 2 was observed for  $H^1$  semi-norm error of the velocity and expected order of 2 was observed for  $L^2$  error of the pressure because of the use of  $Q_1$  elements to interpolate pressure.

1.999635493524672	1.873302176674072	2.832325805975174
2.000330546619946	1.973753558430197	2.978879222764457
2.000030956597092	1.993369649775693	2.996589698011148
2.000003845615942	1.997883037101279	2.999112251694083
2.000001108133545	1.998952202313913	2.999587524766460

$L^2$  norm Pressure

$H^1$  semi norm Velocity

$L^2$  norm Velocity

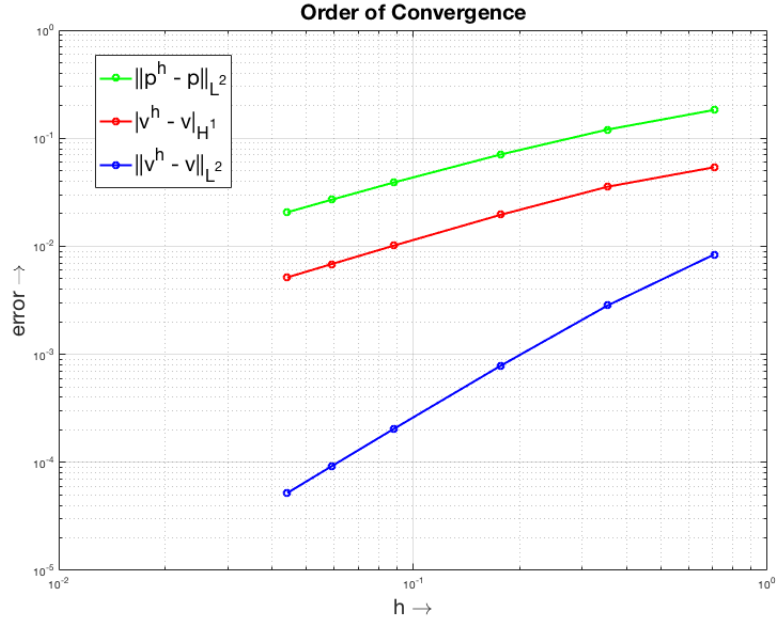


Fig 2. Order of Convergence - Q<sub>2</sub>Q<sub>0</sub> element

**Sub optimal order** of 2 was observed for L<sup>2</sup> error of the velocity because of the use of Q<sub>2</sub> elements to interpolate velocity. **Sub optimal order** of 1 was observed for H<sup>1</sup> semi-norm error of the velocity and expected order of 1 was observed for L<sup>2</sup> error of the pressure because of the use of Q<sub>0</sub> elements to interpolate pressure.

0.603207639658958	0.599564594480739	1.570261149805783
0.764928669723566	0.861079350149105	1.847611293290563
0.859539857030234	0.946183972006160	1.938299914637524
0.908531624097754	0.974407462367428	1.969355957741998
0.930408655436988	0.983754077155205	1.979955365670362

L<sup>2</sup> norm Pressure

H<sup>1</sup> semi norm Velocity

L<sup>2</sup> norm Velocity

## 1.2

GLS stabilization was implemented in order to use non LBB stable elements of first order namely Q<sub>1</sub>Q<sub>1</sub> and P<sub>1</sub>P<sub>1</sub> elements.

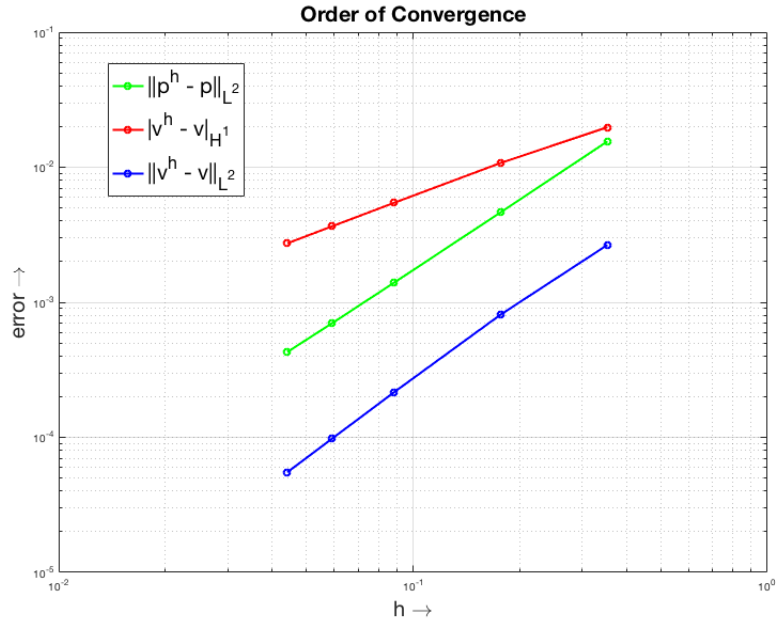


Fig 3. Order of Convergence -  $P_1P_1$  element

Expected order of 2 was observed for  $L^2$  error of the velocity because of the use of  $P_1$  elements to interpolate velocity. Expected order of 1 was observed for  $H^1$  semi-norm error of the velocity and expected order of 2 was observed for  $L^2$  error of the pressure because of the use of  $P_1$  elements to interpolate pressure.

<b>1.743087048803921</b>	<b>0.877747449506963</b>	<b>1.712039935988664</b>
<b>1.731865301828069</b>	<b>0.982035276250644</b>	<b>1.910869797988448</b>
<b>1.716936612119631</b>	<b>0.994044887871000</b>	<b>1.962705036840820</b>
<b>1.686190434792798</b>	<b>0.997873006922521</b>	<b>1.977760564254682</b>

$L^2$  norm Pressure

$H^1$  semi norm Velocity

$L^2$  norm Velocity

## 2

### 2.1

The stokes equations are solved on an uniform Cartesian mesh with 20 elements in each direction for a lid driven cavity problem where the flow is driven by the constant velocity of the top wall.

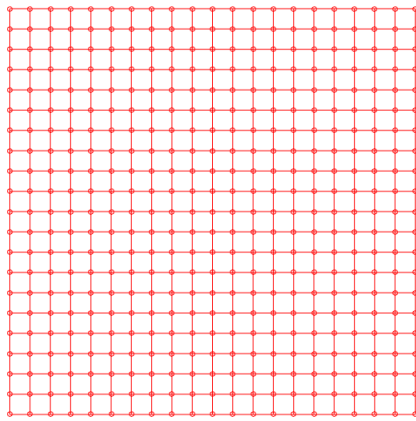


Fig 4a: Uniform Mesh

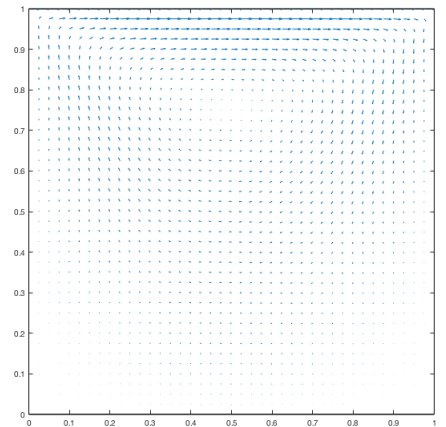


Fig 4b: Velocity Profile

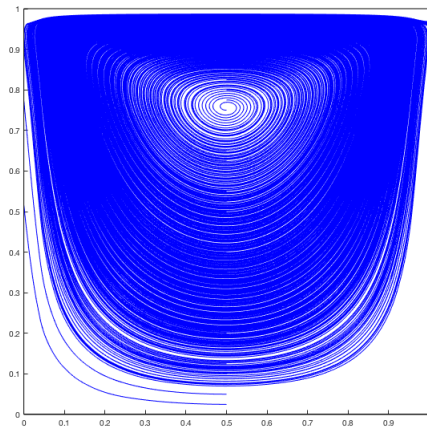


Fig 4c: Velocity streamlines

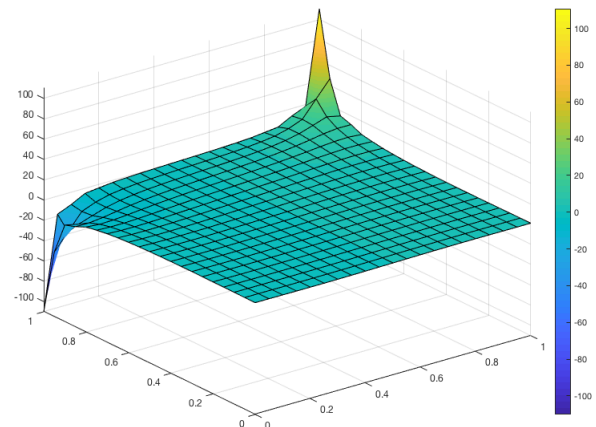


Fig 4d: Pressure Profile

The velocity profile obtained show that the velocity near the upper wall is almost horizontal because of the no slip condition and it causes a vortex structure in the domain. The velocity near the other boundaries are almost zero in accordance with the boundary conditions. The pressure at the top corners tend to go to infinity and because of the coarseness of the mess the behavior is not well captured. There is need to refine the mesh closer to the walls in order to capture the physics better. Hence we go for an adapted mesh with 20 elements on each direction and solve the lid driven cavity problem.

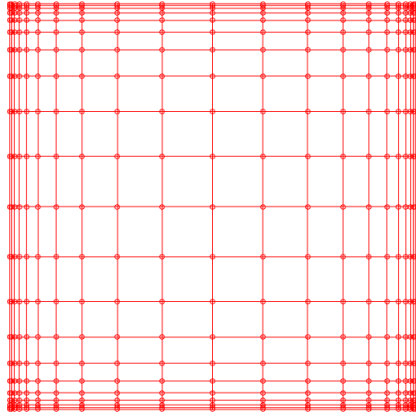


Fig 5a: Adapted Mesh

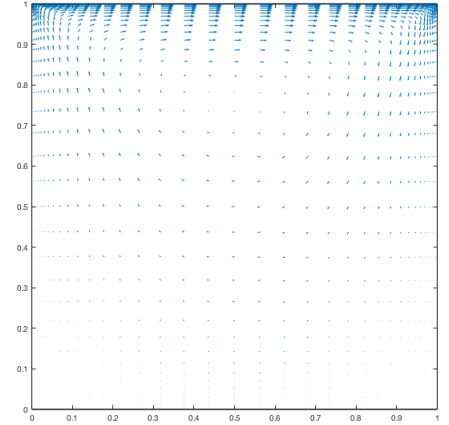


Fig 5b: Velocity Profile

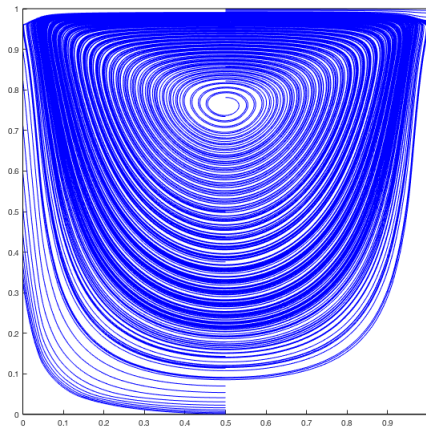


Fig 5c: Velocity streamlines

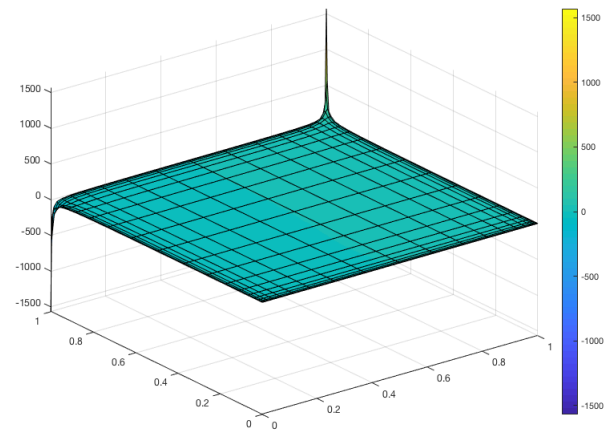


Fig 5d: Pressure Profile

As expected, it can be observed that the adapted mesh captures the physics of the problem at hand better.

## 2.2

The Navier stokes equation was solved using Picard's method for the lid driven cavity problem for  $Re = 100, 500, 1000, 2000$  on an adapted mesh shown previously.

It was observed that for low Reynold's number the stokes solution can be recovered. As the Reynold's number is increased the position of the eye of the vortex moves closer to the center of the domain. It can also be observed that the size of the vortex became bigger with increase in  $Re$ . The peak pressure at the top corners of the domain decreased with increase in  $Re$ .

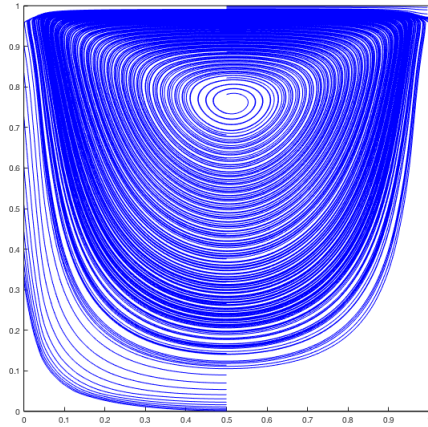


Fig 6a:  $Re = 10$

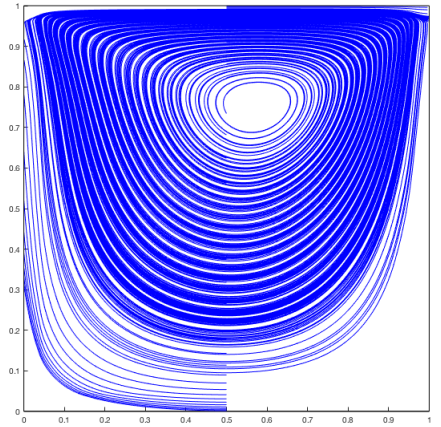


Fig 6b:  $Re = 50$

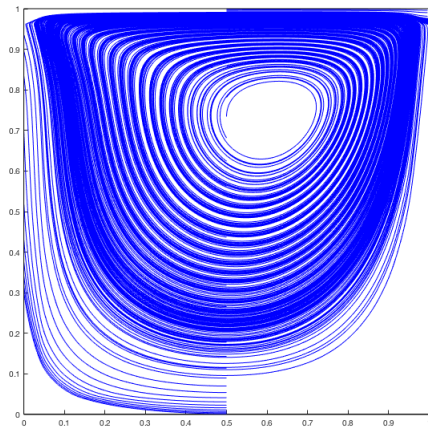


Fig 6c:  $Re = 100$

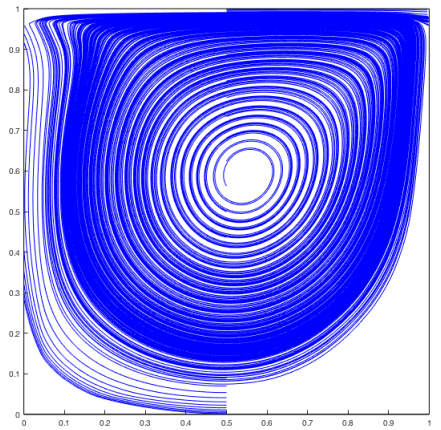


Fig 6d:  $Re = 500$

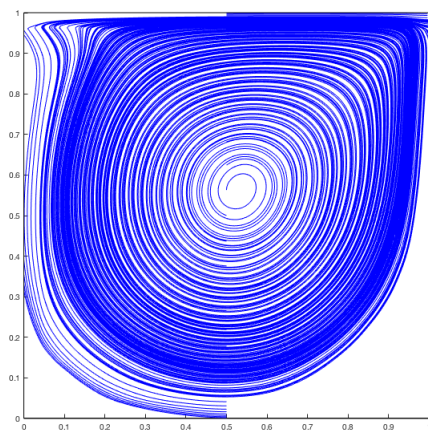


Fig 6e:  $Re = 1000$

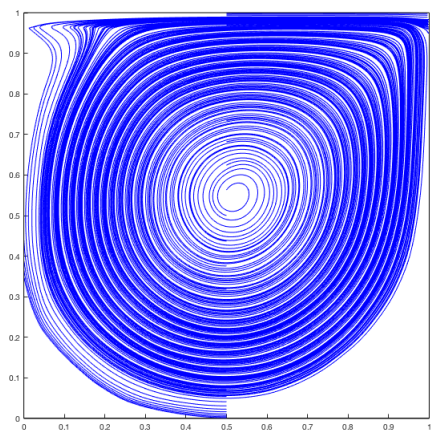


Fig 6f:  $Re = 2000$

It was also observed that the residual decreased in a linear way because of the Picard method. This can prove costly when handling large scale time dependent problems.

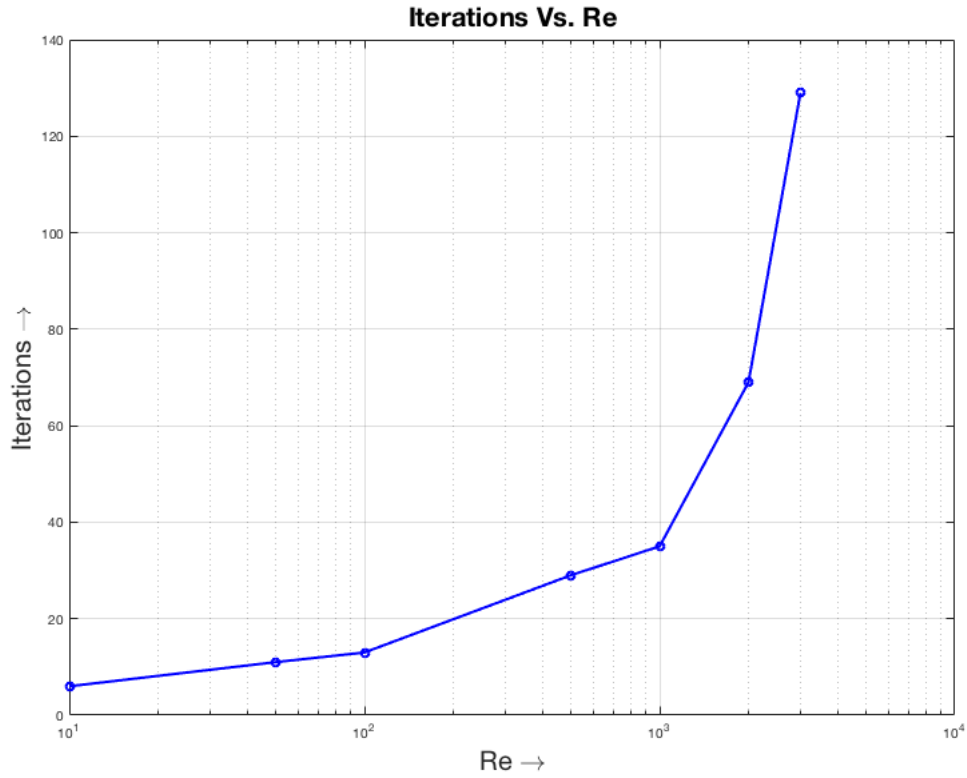


Fig 7: Computational cost Vs Reynold's number

It was also observed that with increase in Re the number of iterations needed to converge grew. This can be attributed towards micro scale instabilities as the Re tends towards the laminar limit into transition and finally the turbulent phase. The Newton Raphson algorithm has to be implemented in order to decrease the number of iterations as it has a rate of convergence of 2. In order to solve problem for higher Re, it is necessary to solve the RANS equations along with a suitable turbulence model for the problem