

FINITE ELEMENTS IN FLUIDS

ASSIGNMENT3- 2D STEADY TRANSPORT PROBLEM

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GLS METHOD

Modified the FEM_system to add GLS method. Pretty straight forward by following the theory in slides-

```
65 - elseif method==3
66 -     %GLS
67 -     Pe = a*h/(2*nu);
68 -     tau_p = h*(1 +9/Pe^2)^(-1/2)/(2*a);
69 -     disp(strcat('Recommended stabilization parameter = ',num2str(tau_p)));
70 -     tau = cinput('Stabilization parameter',tau_p);
71 -     if isempty(tau)
72 -         tau = tau_p;
73 -     end
```

For the loop on gauss points, added a reaction variable, set to zero for the initial computation.

```
144 - elseif method== 3
145 -     reaction=0;
146 -     Ke = Ke + (nu*(Nx'*Nx+Ny'*Ny) + N_ig'*(ax*Nx+ay*Ny) + ...
147 -         ((ax*Nx+ay*Ny)-nu*(Nxx+Nyy)+reaction*N_ig)'...
148 -         *tau*((ax*Nx+ay*Ny)-nu*(Nxx+Nyy))*dvolu;
149 -     f_ig = SourceTerm(aux);
150 -     fe = fe + (N_ig+tau*(ax*Nx+ay*Ny))*(f_ig*dvolu);
151 - end
```

The shape functions provided with the code were incomplete for the double derivatives of the quadratic shape functions wrt ξ and η . The following derivatives were added for $p=2$ for quadrilateral and triangular elements.

Triangular element

```
50 - elseif p ==2
51 -     N = [ xi.*(2*xi-1), eta.*(2*eta-1), (1-xi-eta).*(2*(1-xi-eta)-1),...
52 -         4*xi.*eta, 4*eta.*(1-xi-eta), 4*(1-xi-eta).*xi];
53 -     Nxi = [ 4*xi - 1, zeros(size(xi)), 4*eta + 4*xi - 3,...
54 -         4*eta, -4*eta, 4 - 8*xi - 4*eta];
55 -     Neta = [ zeros(size(xi)), 4*eta - 1, 4*eta + 4*xi - 3,...
56 -         4*xi, 4 - 4*xi - 8*eta, -4*xi];
57 -     N2xi = [ 4*ones(size(xi)), zeros(size(xi)), 4*ones(size(xi)),...
58 -         zeros(size(xi)), zeros(size(xi)), -8*ones(size(xi))];
59 -     N2eta = [ zeros(size(xi)), 4*ones(size(xi)), 4*ones(size(xi)),...
60 -         zeros(size(xi)), -8*ones(size(xi)), zeros(size(xi))];
```

Quadrilateral element

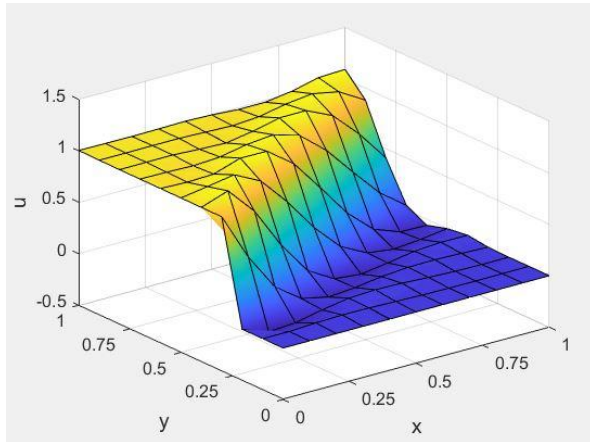
```
16 - elseif p == 2
17 -     N = [xi.*(xi-1).*eta.*(eta-1)/4, xi.*(xi+1).*eta.*(eta-1)/4, ...
18 -         xi.*(xi+1).*eta.*(eta+1)/4, xi.*(xi-1).*eta.*(eta+1)/4, ...
19 -         (1-xi.^2).*eta.*(eta-1)/2, xi.*(xi+1).*(1-eta.^2)/2, ...
20 -         (1-xi.^2).*eta.*(eta+1)/2, xi.*(xi-1).*(1-eta.^2)/2, ...
21 -         (1-xi.^2).*(1-eta.^2)];
22 -     Nxi = [(xi-1/2).*eta.*(eta-1)/2, (xi+1/2).*eta.*(eta-1)/2, ...
23 -           (xi+1/2).*eta.*(eta+1)/2, (xi-1/2).*eta.*(eta+1)/2, ...
24 -           -xi.*eta.*(eta-1), (xi+1/2).*(1-eta.^2), ...
25 -           -xi.*eta.*(eta+1), (xi-1/2).*(1-eta.^2), ...
26 -           -2*xi.*(1-eta.^2)];
27 -     Neta = [xi.*(xi-1).*(eta-1/2)/2, xi.*(xi+1).*(eta-1/2)/2, ...
28 -            xi.*(xi+1).*(eta+1/2)/2, xi.*(xi-1).*(eta+1/2)/2, ...
29 -            (1-xi.^2).*(eta-1/2), xi.*(xi+1).*(-eta), ...
30 -            (1-xi.^2).*(eta+1/2), xi.*(xi-1).*(-eta), ...
31 -            (1-xi.^2).*(-2*eta)];
32 -     N2xi = [eta.*(eta-1)/2, eta.*(eta-1)/2, ...
33 -            eta.*(eta+1)/2, eta.*(eta+1)/2, ...
34 -            -eta.*(eta-1), (1-eta.^2), ...
35 -            -eta.*(eta+1), (1-eta.^2), ...
36 -            -2*(1-eta.^2)];
37 -     N2eta = [xi.*(xi-1)./2, xi.*(xi+1)./2, ...
38 -            xi.*(xi+1)./2, xi.*(xi-1)./2, ...
39 -            (1-xi.^2), -xi.*(xi+1), ...
40 -            (1-xi.^2), -xi.*(xi-1), ...
```

Changes made to make $u=0$ (zero dirichlet boundary) on the outlet boundary, the zero value was assigned to nodes_x1 and nodes_y1 as well.

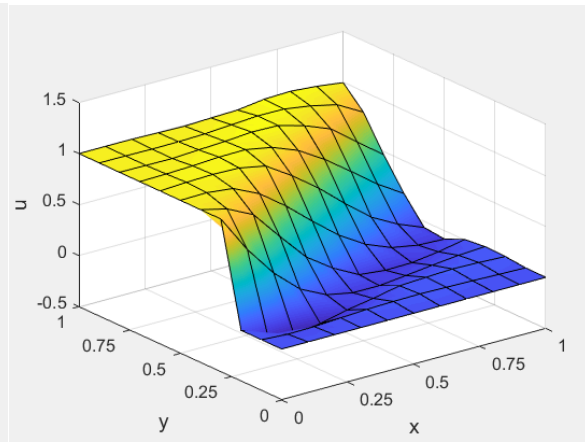
```
66 % nodes on which solution is u=1
67 - nodesDir1 = nodes_x0( X(nodes_x0,2) > 0.2 );
68 % nodes on which solution is u=0
69 - nodesDir0 = [nodes_x0( X(nodes_x0,2) <= 0.2 ); nodes_y0];
70 %for 0 on the outlet boundary
71 % nodesDir0 = [nodes_x0( X(nodes_x0,2) <= 0.2 ); nodes_y0; nodes_x1; nodes_y1];
```

RESULTS

For quadrilateral and triangular elements, the following results are obtained for $p=2$ (quadratic elements) and 5 nodes.



Quadrilateral element, $p=2$



Triangular element, $p=2$

We can see from the results that the code is working for quadratic elements.

Problem variables

The comparisons have been made for both boundary conditions with the following variables

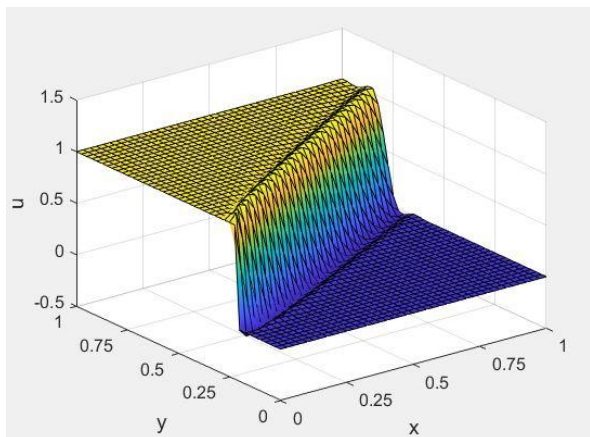
Convection -reaction dominated

$$||a||=1/2, \nu=10^{-4}, \sigma=1$$

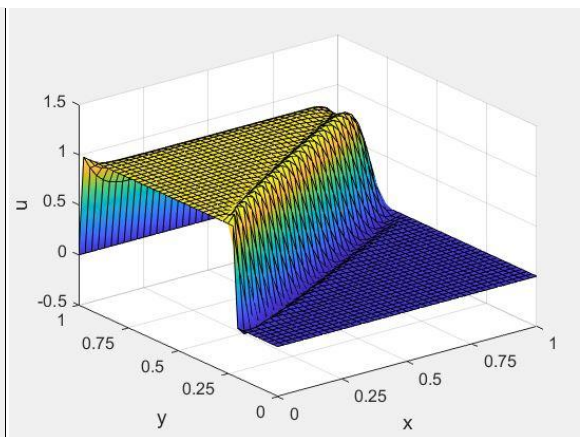
Number of elements in each direction = 20

Quadrilateral element, $p=2$

Method= GLS



Neumann in outer boundary



Zero Dirichlet on the outer boundary

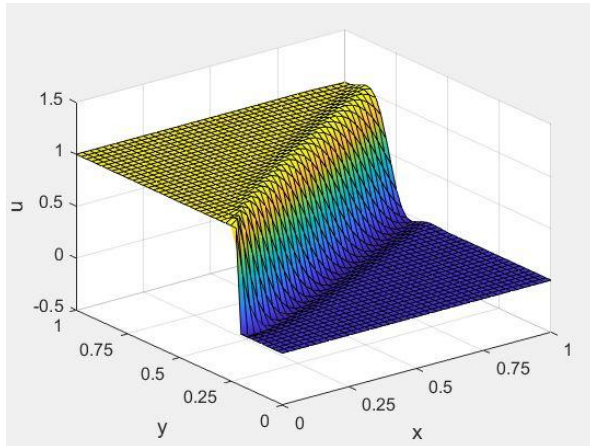
Reaction dominated

$$||a|| = 10^{-3}, \nu = 10^{-4}, \sigma = 1$$

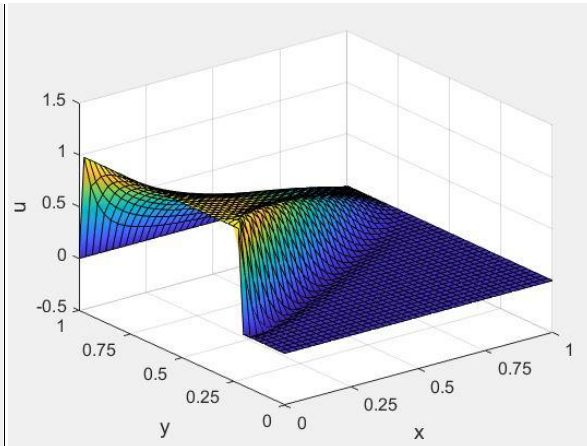
Number of elements in each direction = 20

Quadrilateral element, $p=2$

Method= GLS



Neumann in outer boundary



Zero Dirichlet on the outer boundary

We can see from both the cases, that the reaction dominated simulation gives a smoother profile than the convection-reaction dominated which is in accordance to the theory. The difference is especially prominent for zero dirichlet boundary where the reaction dominated profile gives a smoother transition to zero velocity compared to convection-reaction dominated.